

EFFECT OF Ga ADDITION ON Nd-Dy-Fe-Co-B SINTERED MAGNETS

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To elucidate the effects of Ga addition on Nd-Dy-Fe-Co-B sintered magnets, the temperature dependence of coercivity and changes in the Nd rich phase were studied. The 2nd ferromagnetic phase was observed in Co substituted sintered magnets. The Co containing Nd rich phase, $(\text{Nd, Dy})_3(\text{Co, Fe})$, is changed to $(\text{Nd, Dy})_5(\text{Fe, Co, Ga})_3$ by the Ga addition. iH_c and T_c increase and σ_s decreases with increasing Ga content for synthetic $(\text{Nd}_{0.8}\text{Dy}_{0.2})_5(\text{Fe}_{0.2}\text{Co}_{0.8-u}\text{Ga}_u)_3$ ($0 \leq u \leq 0.6$) alloys. This change of magnetic properties of $(\text{Nd, Dy})_5(\text{Fe, Co, Ga})_3$ seems to be the reason for coercivity enhancement.

1. INTRODUCTION

Coercivity enhancement by Ga addition for $(\text{Nd}_{0.8}\text{Dy}_{0.2})(\text{Fe}_{0.1}\text{Co}_{0.06}\text{B}_{0.08})_{5.5}$ sintered magnets was studied and a 2nd ferromagnetic phase was observed in the temperature dependence of iH_c and AC permeability near T_c ^{1, 2)}. Room temperature iH_c increases by 25% from about 22kOe with Ga addition up to $u=0.015$ for $(\text{Nd}_{0.8}\text{Dy}_{0.2})(\text{Fe}_{0.1}\text{Co}_{0.06}\text{B}_{0.08}\text{Ga}_u)_{5.5}$ sintered magnets. However, room temperature anisotropy field (H_A) does not increase enough to explain the iH_c enhancement by Ga addition, even though 70% of added Ga was found in the 2/14/1 matrix.

In this paper, to understand why Ga addition enhances coercivity, temperature dependence of iH_c near T_c and magnetic properties of the 2nd ferromagnetic phase were investigated.

2. EXPERIMENTAL

Sintered magnets were prepared by the conventional powder metallurgy process and

heat treated according to the pattern described previously³⁾. The iH_c near T_c was measured with a Vibrating Sample Magnetometer (VSM) after magnetization in a 14kOe applied field. For determining the temperature coefficient of iH_c between 25 and 120°C, magnetic properties at 25 and 120°C were measured with a Recording Fluxmeter and VSM, respectively, after magnetization in a 25kOe applied field. EDX/SEM analysis was carried out for a polished surface perpendicular to the alignment direction.

3. RESULTS

Variation of iH_c at 25 and 120°C and the temperature coefficient of iH_c (β , in the temperature range of 25~120°C) with Ga content for $(\text{Nd}_{0.8}\text{Dy}_{0.2})(\text{Fe}_{0.1}\text{Co}_{0.06}\text{B}_{0.08}\text{Ga}_u)_{5.5}$ ($0 \leq u \leq 0.030$) sintered magnet is shown in Fig. 1. The T_2 temperature for each alloy was determined to achieve the lowest irreversible loss ($P_c=2$) at elevated temperatures. iH_c increases up to 0.015 and decreases with increasing Ga content. β decreased with

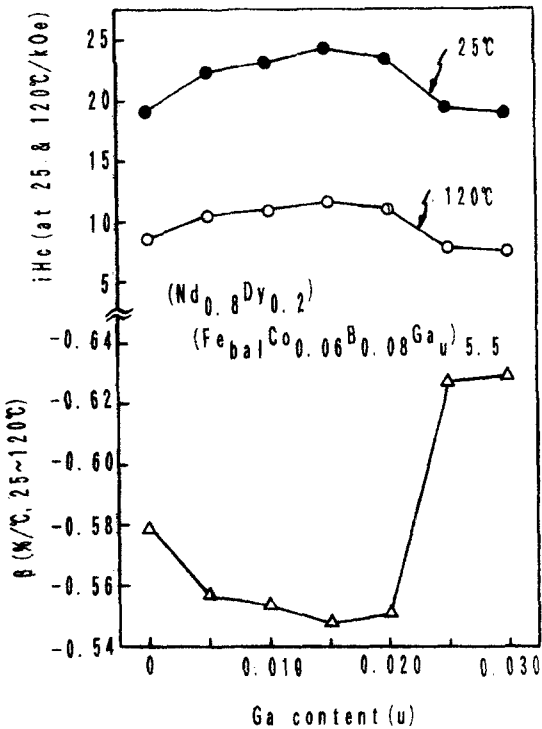


Fig. 1. Variation of iH_c (at 25 and 120°C) and temperature coefficient(β) with Ga content for $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_u)_{5.5}$ ($0 \leq u \leq 0.030$) sintered magnets.

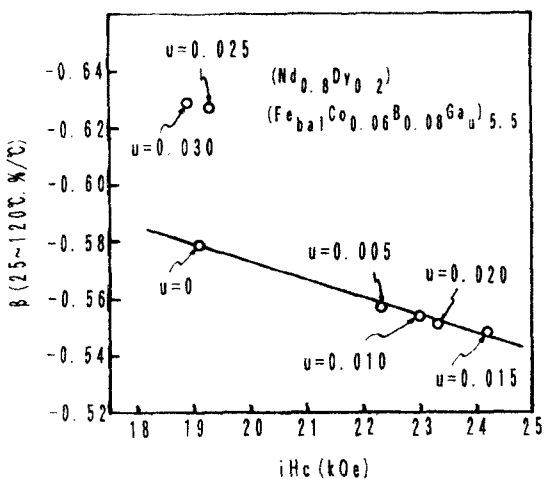


Fig. 2. Variation of β with iH_c for $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_u)_{5.5}$ ($0 \leq u \leq 0.030$) sintered magnets.

increasing iH_c up to $u=0.015$. The lower β is obtained in the specimen with higher iH_c which is attributed to Ga addition as shown in Fig. 2. However, too much Ga addition decreases iH_c and increases β , for example, $u=0.025$ and 0.030 (see Fig. 2). Already, it was observed that the room temperature H_A was not enhanced by Ga addition as was $iH_c^{4)}$. However, there is a possibility that Ga addition changes the temperature dependence of H_A . The temperature dependence of H_A for $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_u)_{5.5}$ ($u=0$ and 0.015) is shown in Fig. 3. No clear difference in the temperature dependence of H_A for sintered magnets with and without Ga addition is observed. There is also no difference in the grain size of the 2/14/1 matrix which

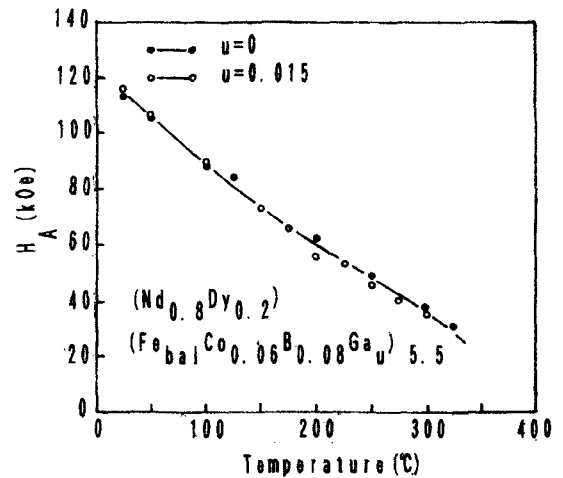


Fig. 3. Temperature dependence of H_A for $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_u)_{5.5}$ ($u=0$ and 0.015) sintered magnets.

contains 70% of the added Ga⁴⁾.

Fig. 4 shows the variation of iH_c near T_c for (1) $Nd(Fe_{0.92}B_{0.08})_{5.4}$, (2) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08})_{5.5}$, (3) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08})_{6.2}$ and (4) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_{0.015})_{5.5}$ sintered magnets. For Nd-Fe-B ternary sintered magnet, T_c of the matrix is 310°C and no 2nd ferromagnetic phase was observed. Also, for high z magnet, alloy (3) ($z=TM/RE$, $TM:Fe+Co+B+Ga$, $RE:Nd+Dy$), T_c of the matrix is 380°C

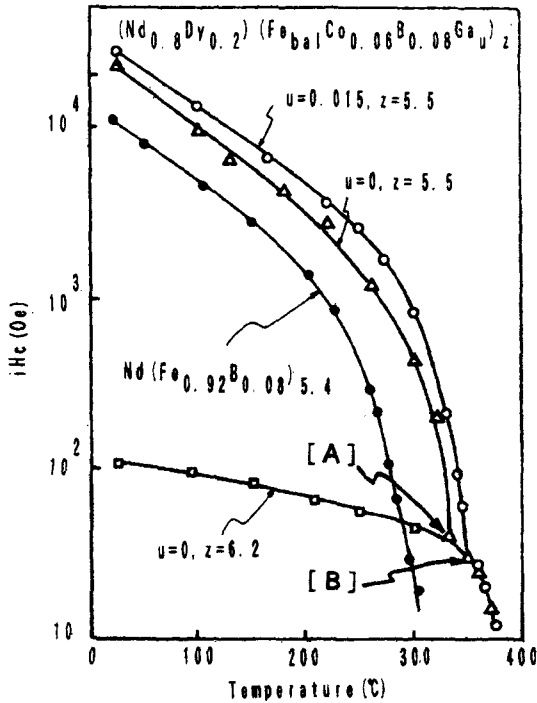


Fig. 4. Variation of iH_c near T_c for
 (1) $Nd(Fe_{0.92}B_{0.08})_{5.4}$,
 (2) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08})_{5.5}$,
 (3) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08})_{6.2}$ and
 (4) $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_{0.015})_{5.5}$
 sintered magnets.

and no 2nd ferromagnetic phase is observed. For the Co substituted sintered magnets with high iH_c , alloys (2) and (4), T_c of the matrix and 2nd ferromagnetic phase are observed. The point of intersection of two iH_c vs T curves for alloys (2) and (3), which is $330^\circ C$ (point [A] in Fig. 4), is thought to be

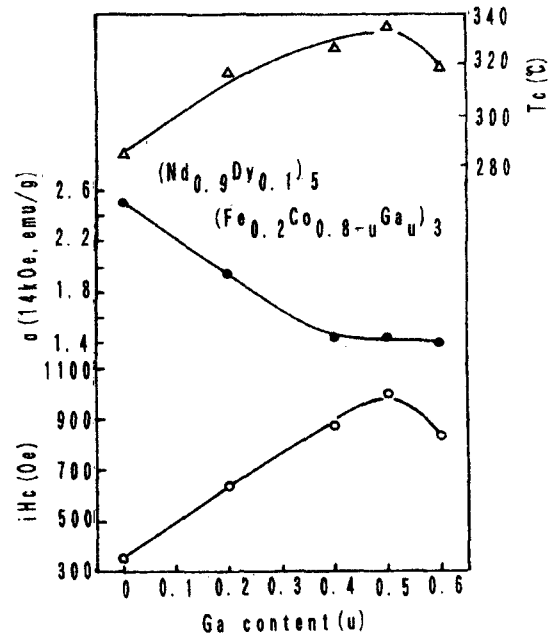


Fig. 5. Variation of σ_s , iH_c and T_c with Ga content for $(Nd_{0.9}Dy_{0.1})_5(Fe_{0.2}Co_{0.8-u}Ga_u)_3$ ($0 \leq u \leq 0.6$) alloys.

the T_c of the 2nd ferromagnetic phase. T_c 's of the matrix are 380 and $385^\circ C$ for alloys (2) and (4), respectively. T_c 's of the 2nd magnetic phase are 330 and $350^\circ C$ (point [B] in Fig. 4) for alloys (2) and (4), respectively.

Ga also exists in the boundary phases, namely Nd rich phases. The results of EDX/SEM analysis is shown in Table 1. There are 2 kinds of Nd rich phases, Co free and Co containing Nd rich phase. The Co containing Nd rich phases is $(Nd,Dy)_3(Co,Fe)$. This phase

Table 1. Phase analysis with EDX/SEM for $(Nd_{0.8}Dy_{0.2})(Fe_{ba1}Co_{0.06}B_{0.08}Ga_u)_{5.5}$ ($u=0$ and 0.015) sintered magnets. (at.%)

u	Phase	Nd	Dy	Fe	Co	Ga	Remarks
0	2/14/1	8.5	2.9	81.0	7.6	---	
	1/4/4	13.6	6.2	74.6	5.6	---	
	Nd rich	74.6	14.4	11.0	---	---	Co free Nd rich
	Nd rich	71.4	2.6	5.7	20.3	---	Co containing Nd rich(3/1)
0.015	2/14/1	8.6	3.8	80.0	7.2	0.2	
	1/4/4	13.3	6.6	74.5	5.6	---	
	Nd rich	70.1	14.8	15.1	---	---	Co free Nd rich
	Nd rich	57.1	4.4	7.2	7.2	24.1	Co containing Nd rich(5/3)

Table 2. Curie temperatures(T_c) of matrix and the 2nd ferromagnetic phases for R-TM-B sintered magnets.

Composition	Matrix and its T_c	The 2nd ferromagnetic phase and its T_c
Nd(Fe _{0.92} B _{0.08}) _{5.4}	Nd ₂ Fe ₁₄ B $T_c=310^\circ\text{C}$	none
(Nd _{0.8} Dy _{0.2})(Fe _{0.86} Co _{0.06} B _{0.08}) _{5.5}	(Nd, Dy) ₂ (Fe, Co) ₁₄ B $T_c=380^\circ\text{C}$	(Nd, Dy) ₃ (Co, Fe) $T_c=330^\circ\text{C}$
(Nd _{0.8} Dy _{0.2})(Fe _{0.845} Co _{0.06} B _{0.08} Ga _{0.015}) _{5.5}	(Nd, Dy) ₂ (Fe, Co, Ga) ₁₄ B $T_c=385^\circ\text{C}$	(Nd, Dy) ₅ (Ga, Co, Fe) ₃ $T_c=350^\circ\text{C}$

is changed to (Nd, Dy)₅(Ga, Co, Fe)₃⁵⁾ by Ga addition. The Ga is condensed in the Co containing Nd rich 5/3 phases. The T_c of the matrix and the 2nd ferromagnetic phases for R-TM-B sintered magnets are tabulated in Table 2. Using the results of EDX/SEM analysis, Co containing alloys were arc melted. The variation of magnetic properties and T_c with Ga content for (Nd_{0.9}Dy_{0.1})₅(Fe_{0.2}Co_{0.8-u}Ga_u)₃ ($0 \leq u \leq 0.6$) alloys is shown in Fig. 5. iH_c and T_c increase with increasing Ga content with the maximum at $u=0.5$. However, σ_s (magnetization at 14kOe) decreases linearly up to $u=0.4$, and then keeps constant. Ga addition to the Co containing Nd rich phase decreases σ_s and increases T_c . This change of magnetic properties of the Co containing Nd rich phase seems to be the reason for coercivity enhancement of sintered magnets. The co-existing of matrix and (Nd, Dy)₅(Ga, Co, Fe)₃ phases and some pinning force defined at the interface of these phases seems to be the origin of the high iH_c . Another possibility is that the decrease in σ_s of the 5/3 phase suppresses its behavior as nucleation sites.

4. SUMMARY

The effect of Ga addition for Nd-Dy-Fe-Co-B sintered magnets was studied to understand the coercivity enhancement. The Co containing Nd rich phase, (Nd, Dy)₃(Co, Fe), is

observed in the Nd-Dy-Fe-Co-B sintered magnets. This phase is changed to (Nd, Dy)₅(Ga, Co, Fe)₃ by Ga addition. T_c 's of the 2nd ferromagnetic phases were observed at 330°C and 350°C in the temperature dependence of iH_c near T_c for sintered magnets with and without Ga addition, respectively. So, the 2nd ferromagnetic phase should be (Nd, Dy)₃(Co, Fe) and (Nd, Dy)₅(Ga, Co, Fe)₃ for Ga free and Ga containing sintered magnets. T_c increases and σ_s decreases with increasing Ga content for the (Nd, Dy)₅(Fe, Co, Ga)₃. This change of the magnetic properties of the Co containing Nd rich phase seems to contribute to the coercivity enhancement of Nd-Dy-Fe-Co-B-Ga sintered magnets.

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