# Simultaneous Reduction of SOx and NOx in Manganese Oxides Particle Bed

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The present study is concerned with simultaneous reduction of SOx and NOx for dry gas cleaning of exhaust gas. Manganese oxides has a possibility of a reducing agent for De-SOx and De-NOx reactions. The simultaneous De-SOx/NOx experiments were conducted under common operation conditions.

From simultaneous De-SOx/NOx experiments, it was found that manganese oxides had the dual functions of De-SOx and De-NOx. The reducing efficiencies of simultaneous De-SOx/NOx were almost equal to those of individual De-SOx and De-NOx operations. Under high temperature region (573-673K), the extent of SO2 removal efficiency for simultaneous De-SOx/NOx operations was higher than that obtained from the individual De-SOx operation. This high De-SOx effect might be attributed to the existence of water vapor which was produced by the reaction between O2 and NH3 which were injected for selective catalytic reduction of NOx.

The emission level of NOx was kept lower under the simultaneous De-SOx/NOx operations, even when the O2 concentration was as high as that of the case where the De-NOx experiment was individually conducted. key words: simultaneous De-SOx/NOx, manganese oxides, activated manganese oxide, selective catalytic reduction

# 1. INTRODUCTION

The emission of sulfur oxides (SOx) and nitrogen oxides (NOx) through the combustion of fossil fuels in combustors and furnaces are related to the cause of environmental disasters such as acid rain and photochemical smog. In order to remove these acid gases, many gas cleaning technologies have been developed and carried out. Although these endeavors have resulted in the present low emission level, it is worthwhile to achieve zero emission process in order to protect the environment for future generation.

At present, De-SOx and De-NOx operations for exhaust gas have been carried out separately. SOx is generally removed by injecting CaCO3 into the combustor or ventilating the exhaust gas through an alkaline slurry. On the other hand, NOx is usually removed by selective catalytic reduction (SCR) or selective non-catalytic reduction (SNCR) with appropriate reducing agents. However, advanced studies for development of much effective and advantageous De-SOx/NOx process have been conducted. In recent years, adsorption and catalytic reduction by activated carbon, electron beam flue gas treatment [1] and combination of sorbent injection and selective non-catalytic reduction [2] have been developed and used experimentally as simultaneous De-SOx/NOx processes.

This present study is concerned with the applicability of simultaneous reduction of SOx and NOx by using manganese oxides. According to various reports, manganese oxides react with SO2 in the exhaust gas to form manganese sulfate [3-5]. It was found that DeSOx capacity of manganese oxides enhanced under the presence of water vapor. On the other hand, it is well known that some metal oxides can work as catalysts of selective catalytic reduction (De-NOx operations). Previous paper reported that selective catalytic reduction with reducing agent CH3OH (by using alumina as a catalyst) has NOx conversion under 673K and CH3OH/NOx mole ratio = 2[6]. For simultaneous De-SOx/NOx operations, several metal oxides supported on silica or alumina are used for gas cleaning. As a one of recent researches, copper oxide on silica was investigated the possibility of a reducing agents for simultaneous De-SOx/NOx operations[7],[8]. From these reports, copper oxide for SOx removal can be recycled by the regeneration process, but De-NOx reactivity of CuSO4, produced by the desulfurization, became lower, compared to that of V2O5.

In this research, we evaluated the De-SOx capacity and De-NOx reactivity of two manganese samples (Manganese Type I & II) and focused on the effect of temperature and O2 concentration for Manganese Type I on simultaneous De-SOx/NOx.

# 2. EXPERIMENTAL SECTIONS

### 2.1 Reaction

In the process of simultaneous De-SOx/NOx by using manganese oxides, the absorption of sulfur dioxide by MnO2 can be described by following stoichometric equation.

$$MnO_2 \cdot iH_2O + SO_2 \rightarrow MnSO_4 + iH_2O$$
(1)

We used this equation to calculate De-SOx capacity, the conversion of MnO2 to MnSO4, XDe-SOx:

$$X_{\text{DeSOx}} [\%] = \frac{\frac{\Delta W}{W_0}}{\frac{W_{\text{MnO2}}}{W_{\text{MnO2}}}} \times 100} \times \frac{\sqrt{\frac{M_{\text{MnO2}}}{W_{\text{MnO2}}}}}{M_{\text{MnO2}}}$$
(2)

On the other hand, the selective catalytic reduction can transforms NOx to N2 and H2O by using reducing agents. As for this NOx reduction processes, in the presence of O2, the reaction equations of NOx reducing will be different from those in the absence of O2.

(I) In the absence of O2  

$$6NO + 4NH3 \rightarrow 5N2 + 6H2O$$
 (3  
 $(NO + 2NH2 \rightarrow 7H2 + 12)H2O$  (4)

 $4NO + 4NH_3 + O_2 \rightarrow 4N_2 + 6H_2O$  (5)

$$2NO_2 + 4NH_3 + O_2 \rightarrow 3N_2 + 6H_2O$$
 (6)

For evaluating De-NOx reactivity, we defined NOx removal efficiency.

$$De-NOx [\%] = \frac{[C]_{initial} - [C]_{final}}{[C]_{initial}} \times 100$$
(7)

# 2.2 Experiments

Figure 1 shows a pyrex tubular flow reactor with an electric furnace for simultaneous De-SOx/NOx experiments. A distributor plate is located above the preheating zone at 900 mm height in the reactor for setting the sample in the reactor. After raising the temperature of the apparatus to a desired value, the simulated gas mixture with total flow rate 6.6 cm3/sec was introduced into the reactor tube from the bottom. Then the experiment was started by setting the sample in the reactor.

The composition of the mixing simulated gas was controlled by calibrated flow meters. The concentrations of SOx and NOx in the outlet gas were measured by ultra-red spectroscope SOx meter and chemiluminescence NOx meter.



#### 2.3 Samples

The chemical compositions and surface area of manganese samples that we used in these experiments are described in Table I. These manganese samples are ores that were produced at different mines. We crushed and screened these manganese ores, and prepared them to adjust the particles size with 1 mm diameter in the present experiments.

Table I	Chemical	compositions & surface area
		of manganese samples

					*	0	-
	MnO2	Al203	FeO	Fe2O3	SiO <sub>2</sub>	Bond Water	Surface Area
Manganese Type I	65.9	7.76	2.73	1.82	1.69	7.00	18.83
Manganese Type II	69.0	0.01	0.22	13.34	6.07	2.92	5.83
	diameter	[ wt %	] [m²/g]				

#### 3. RESULTS AND DISCUSSION

3.1 De-SOx capacity and De-NOx reactivity of two manganese samples

Figure 2 shows the outlet SO2/NOx concentration in simultaneous De-SOx/NOx experiments by using two manganese samples. The experiments were conducted at 573K with gas mixture containing 200 ppm SO2, 200 ppm NOx, 200 ppm NH3, 5% O2 and Ar balance. We found that the outlet SO2 concentration dropped



(temp. : 573K; O2 concentration: 5%; Manganese Type I (a) & Type II (b))

from 200 ppm to about 170 ppm even when the reactor was not charged with manganese sample. This may be attributed to the formation of sulfur based acids which might be produced by the reaction between SO2 and H2O derived from NH3 oxidation. It was seen from Figure 2 that manganese oxides had the dual functions of SO2 and NOx removal from the simulated gas. Moreover, De-SOx capacity and De-NOx reactivity became almost equal to that of individual De-SOx or De-NOx experiments.

In desulfurization period, the outlet SO2 concentrations increased as time passed for both two manganese samples. However, the outlet concentration of NOx was not so much changed during experiments. One of the reasons why the above phenomenon took place is that iron oxides in the manganese samples might work as a catalyst for selective catalytic reduction with NH3.

It was confirmed by SEM/EDS analysis that sulfur molecules were trapped onto manganese molecules for both two manganese samples employed. The sulfur was not observed on iron molecule. As for two manganese samples, it was indicated from Figure 2 that Manganese Type I had greater De-SOx capacity and De-NOx reactivity, compared with Manganese Type II. This result is explained by a larger surface area of Type I. The surface area of Manganese Type I is more than three times larger than that of Manganese Type II. 3.2 De-SOx capacity

As for De-SOx capacity in simultaneous De-SOx/NOx experiments, the effect of temperature, 473, 573, 673K is shown in Figure 3. In this figure, the results of individual De-SOx experiments are described to compare with other experimental results. It was observed that the outlet SO2 concentrations are almost same value at 473 and 673 K. On the contrary, we found the great difference of outlet SO2 concentration



Fig.3 Time vs.outlet SO2 concentration (temp.: 473-673K; O2 concentration: 5%; ManganeseType I)

on 573 K. The obtained value of simultaneous De-SOx/NOx experiment was much better than that of individual De-SOx experiment.

To explain the above results shown in Figure 3, we employed thermogravimetric analyzer to measure the weight change in both dry and wet De-SOx experiments. Figure 4 shows the influence of temperature on the conversion attained at 35 min for both dry and wet De-SOx experiments. In the presence of H2O, the reaction between MnO2 and SO2 can be described as follows :

$$SO_2 + H_2O \rightarrow H_2SO_3 \tag{8}$$
$$MnO_2 + H_2SO_3 \rightarrow MnSO_4 + H_2O \tag{9}$$

In the absence of H2O, the absorption of SO2 by MnO2 occur as Equation (1). Then, the final product obtained through both reaction paths is MnSO4 in these experiments. To evaluate SOx absorption capacity, we used equation (2) to calculate the conversion MnO2 to MnSO4. It was seen that the conversion in the presence of water vapor is better than that in the absence of water vapor at all temperatures. This enhancement in reactivity of MnO2 toward SO2 under the presence of water vapor is considered to be affected by the formation of sulfur based acids. In simultaneous De-SOx/NOx experiments, water vapor was produced from the oxidation of NH3 as a reducing agent of selective catalytic reduction. The presence of water vapor enhanced De-SOx capacity of manganese oxides in simultaneous De-SOx/NOx experiments. 3.3 De-NOx reactivity

Figure 5 shows the effect of temperature on De-NOx reactivity of Manganese Type I under O2 concentration 5 or 15%. It was seen that the difference of De-NOx reactivities on both individual De-NOx and simultaneous De-SOx/NOx experiments is not clearly at lower temperature. On the contrary, at higher temperature, De-NOx reactivity on simultaneous De-



Fig.4 Effect of water vapor on MnO2 conversion into MnSO4 after 35min reaction (tested by Thermogravimetric Analyzer)



on De-NOx reactivity of Manganese Type I



on De-NOx reactivity of Manganese Type I

SOx/NOx experiments was over two times that on individual De-NOx experiments. This phenomenon that De-NOx reactivity on simultaneous De-SOx/NOx experiment is higher than that on individual De-NOx experiment was illustrated in previous paper [9]. The same trend was observed from the results with the O2 concentration of 5 and 15%.

Figure 6 shows the effect of O2 concentration De-NOx reactivity at simultaneous De-SOx/NOx experiments. From this figure, we found that De-NOx reactivity in simultaneous De-SOx/NOx experiments was enhanced, compared with the results of individual De-NOx experiments at higher O2 concentration. The maximum NOx removal efficiency was observed at about 7% O2 on individual De-NOx experiments. On the other hand, in simultaneous De-SOx/NOx experiments, the maximum efficiency became over 90% at about 10% O2.

## 4. CONCLUSION

Based on De-SOx/NOx experimental results, it can be summarized as :

Simultaneous De-SOx/NOx experiments indicated that manganese oxides has the dual functions of removing SOx and NOx with values almost equal to that of the individual De-SOx and De-NOx processes.

As for De-SOx capacity, it was cleared that the MnO2 conversion to MnSO4 will be enhanced in the presence of water vapor, which was produced by the oxidation of NH3. As a result, the outlet SO2 concentrations in simultaneous De-SOx/NOx experiments were lower than that in individual De-SOx experiments.

On the other hand, MnO2 has equal or greater activity, compared with the obtained results from individual De-NOx experiments. Especially, it was observed that at higher temperature and O2 concentration De-NOx reactivity is greater enhanced.

### 5. NOMENCLATURE

 $\Delta W[g]$ :weight gain of the sample upon sulfurization W[g]: initial weight of sample

 $WMnO_2$  [-]:weight fraction of manganese oxide in sample

MMnO2 [-]:molecular weight of MnO2

MMnSO<sub>4</sub> [-]:molecular weight of MnSO<sub>4</sub>

[C]initial [ppm]:initial concentration of NOx

[C]final [ppm]:final concentration of NOx

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